

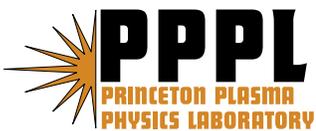
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# Design, installation and performance of the new insulator for NSTX CHI experiments

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**Abstract**— Coaxial Helicity Injection (CHI), a non-inductive method to initiate plasma and generate toroidal plasma current, is being investigated in the National Spherical Torus Experiment (NSTX). The center stack and outer vacuum vessel are separated by insulating gaps at the top and bottom of the slim central column so that a high voltage (up to 2 kV) can be applied between them from a pulsed power supply or a capacitor bank to initiate an arc discharge. In the presence of a suitable poloidal magnetic field, the discharge is initiated at the lower gap (the injector gap) and because of the strong toroidal field develops a helical structure resulting in substantial toroidal plasma current being driven. In NSTX, up to 390 kA of toroidal current has been generated for an injected current of 25 kA. The early investigations of CHI however frequently developed arcs across the insulator at the top of the machine (the absorber gap), which terminated the desired discharge. This arcing greatly restricted the operational space available for CHI studies. During 2002, the absorber region was modified to suppress these arcs. The new design includes a new ceramic insulator on the high field side of the absorber region with a much longer tracking distance between conducting elements at the different potentials. Furthermore, two new coils were installed near the absorber to provide the ability to minimize the poloidal field connecting the center stack and outer vacuum vessel. During the subsequent experimental campaign, CHI operation was less prone to arcing in the absorber and those arcs that did occur did not terminate the main discharge.)

**Keywords**- Coaxial Helicity Injection, Spherical Torus

## I. INTRODUCTION

Because of the limited space in a spherical torus to accommodate an internal inductive coil, an essential feature of future spherical torus designs will be the inclusion of an effective means to initiate the plasma and to drive plasma current without relying upon inductive drive. Coaxial Helicity Injection (CHI) has been shown to be effective for initiation and for ramp-up on the Helicity Injected Torus (HIT)[1], the Helicity Injected Torus-II (HIT-II)[2] and the National Spherical Torus Experiment (NSTX)[3] to drive up to 390 kA of toroidal current[4]. More recently, the existence of persistent plasma current on closed poloidal flux surfaces after

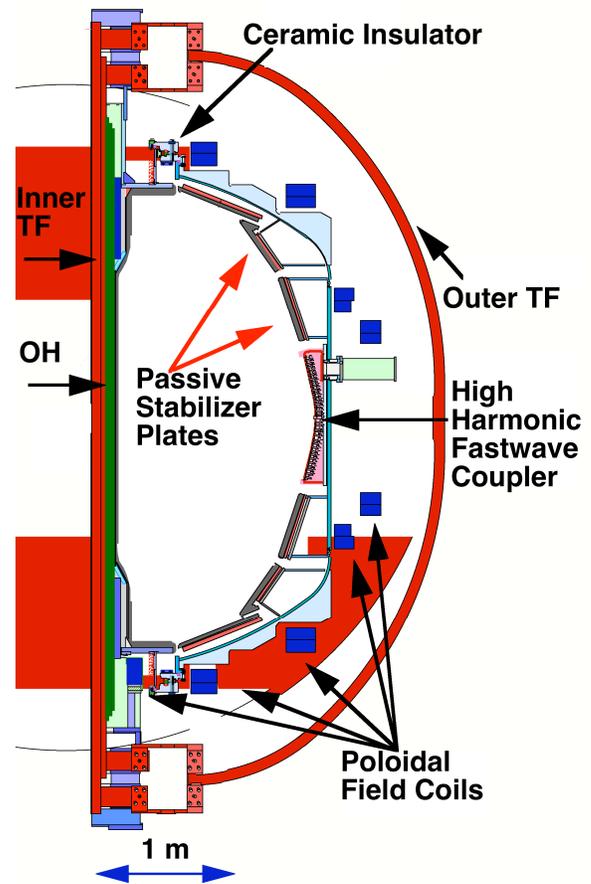


Figure 1. Cross-section of NSTX.

the CHI drive is turned off has been observed on both HIT-II[5,6] and NSTX[7]. Fig. 1 shows the configuration of NSTX. In CHI experiments, the center column is insulated from the outer vacuum vessel and a discharge between the outer vessel and the center column is initiated by providing a high voltage between them with either a power supply or a capacitor bank. During CHI, the inner and outer vessels are linked by poloidal flux at the bottom of the machine, the injector region, provided

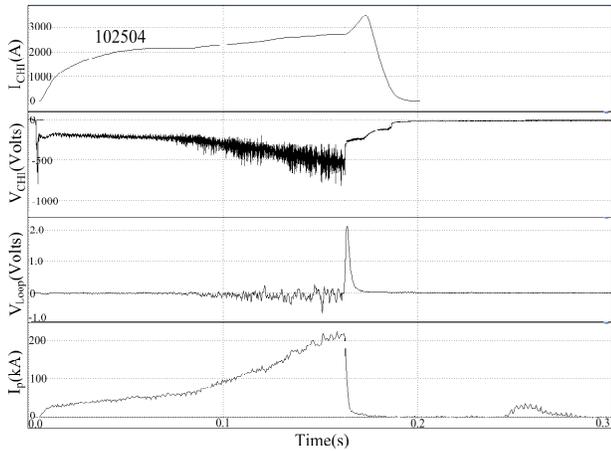


Figure 2. Low impedance absorber arc cause  $I_{CHI}$  to increase rapidly and  $I_p$  to terminate. Note the lack of noise on the  $V_{CHI}$  during the arc.

by the poloidal field coils, the toroidal coils provide a field that by itself would insulate the inner and outer vessel from each other. The net result is that the field lines connect the inner and outer walls over a helical path so that current flowing on those field lines will result in both poloidal current ( $I_{CHI}$ ) and toroidal current ( $I_p$ ), typically the ratio of the fields is such that  $I_p/I_{CHI}$  is around 10. The direction of the poloidal and toroidal fields and CHI injector voltage are chosen so that the  $\mathbf{E} \times \mathbf{B}$  direction is up into the main chamber. Discussion of the CHI discharge evolution by magnetic reconnection from a helical arc on open field lines to a plasma with its current flowing on closed poloidal flux surfaces is beyond the scope of this paper. The reader is referred to [8] through [11] and references cited therein for further discussion on CHI discharge evolution.

## II. ISSUE

As the plasma drifts up, poloidal flux from  $I_p$  links the inner and outer vessel at the top of the machine, the absorber region, and plasma drifting up into the absorber region provides a medium through which current can flow. This can allow an arc to form in the absorber region, which is deleterious to the desired discharge. Fig. 2 shows traces of  $I_{CHI}$ , the applied injector voltage  $V_{CHI}$ , the measured loop voltage,  $V_{Loop}$ , and  $I_p$  for a discharge taken in 2002 in which an absorber arc occurred at about 0.163 ms. Signatures of the absorber arc include a rapid increase in  $I_{CHI}$ , reduced noise on  $V_{CHI}$  and rapid termination of  $I_p$ . Fisheye TV camera views of the discharge taken at 0.162 and 0.165 s, just before and during the arc are shown in Fig. 3. Note the helical structure seen at 0.162 s, which indicates current flowing along spiral field lines. At 0.165 s, during the arc, the main discharge has all but disappeared from the TV picture and a bright, poloidally and toroidally localized arc is seen. The local non-axisymmetric nature indicates the possibility of an arc along a material surface. Such arcs have the potential to damage the machine and prevent CHI from being effectively applied. The avoidance of such arcs was difficult, they occurred on about 2/3 of all CHI discharges before 2002, despite concerted efforts to find scenarios that would avoid their occurrence.

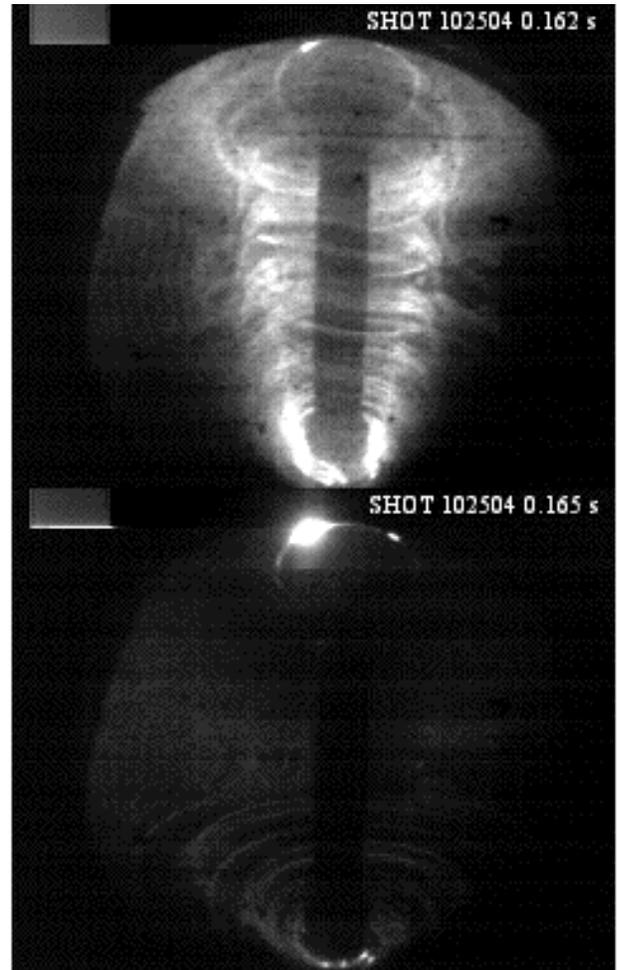


Figure 3. TV images before and during an absorber arc in NSTX before the insulator redesign.

## III. SOLUTION

In order to make NSTX more resistant to these absorber arcs, the absorber region was redesigned in 2002 based upon experience from HIT[1], HIT-II[2] and General Atomics DIII-

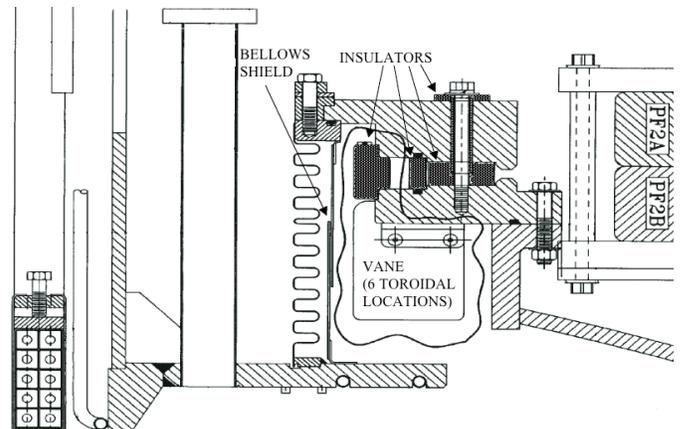


Figure 4. Design detail of absorber region of NSTX prior to 2002.

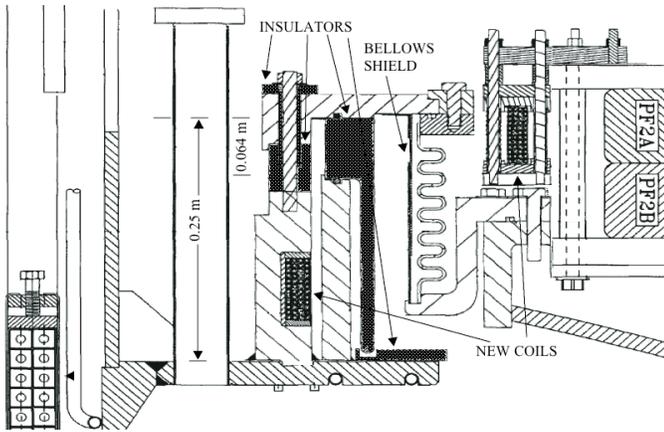


Figure 5. New absorber design in NSTX. Note the much larger insulator in the new design.

D[12] to provide an insulator on the high field side of the absorber with a much longer tracking distance between conductors. The redesign provided the opportunity to install poloidal field coils near the insulator that could be energized to minimize the poloidal field connecting the inner and outer vessel in the absorber region should that be necessary.

Fig. 4 shows the old insulator design with the insulator on the low toroidal field side of the absorber region and a short distance between the conducting surfaces. That is to be contrasted with the new design with a much longer insulating surface between the conductors at inner and outer vessel potentials shown in Fig. 5. The alumina insulator in the new design has a total height of 0.25 m and 0.0636 m between vacuum surfaces. There is also a split ceramic skirt to cover the metallic surface at the bottom of the absorber region.

After the new insulator was installed, the incidence of absorber arcs was reduced and when the arcs did occur, they had higher impedance and did not terminate the main discharge. Fig. 6 shows a shot taken with the new insulator, I<sub>CHI</sub> increases when the arc occurs and I<sub>p</sub> is reduced, but not eliminated. Fig. 7 has TV images before and during the arc.

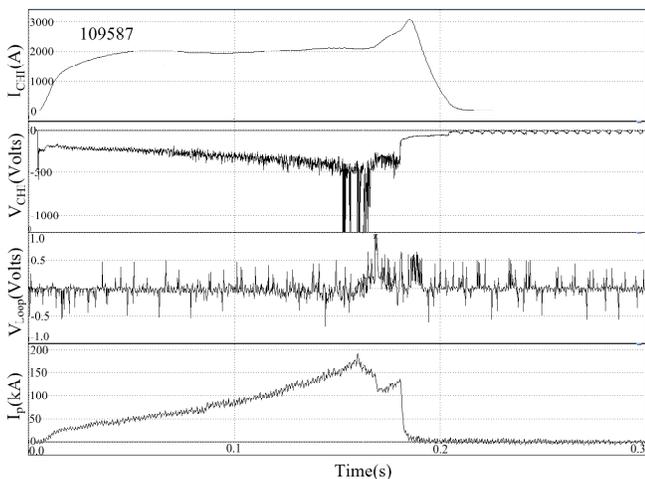


Figure 6. Absorber arc with new insulator. Note that even during the arc when I<sub>CHI</sub> is increasing rapidly that the main discharge, I<sub>p</sub>, is not terminated and the hash in V<sub>CHI</sub> indicates a variable plasma load.

With the new design, it is typical that absorber arcs do not exhibit the bright, localized light seen with the previous design, but either a diffuse ring at the top of the machine or very little visible light as in this case. There has been no evidence that any damage occurred when the insulator was inspected during an opening following the run.

Since the insulator has performed well, there has been no need to use the new poloidal field coils and they remain as a backup in case a scenario is found where their use might be required.

#### IV. SUMMARY

The new insulator design has performed well. The frequency of low impedance absorber arcs that terminate the main discharge has been dramatically reduced. This has permitted greater flexibility in operations, which has facilitated significant improvements in CHI operation on NSTX as evidenced by the recent results in [7]. The insulator has performed well enough that so far there has been no need to implement the new field nulling coils.

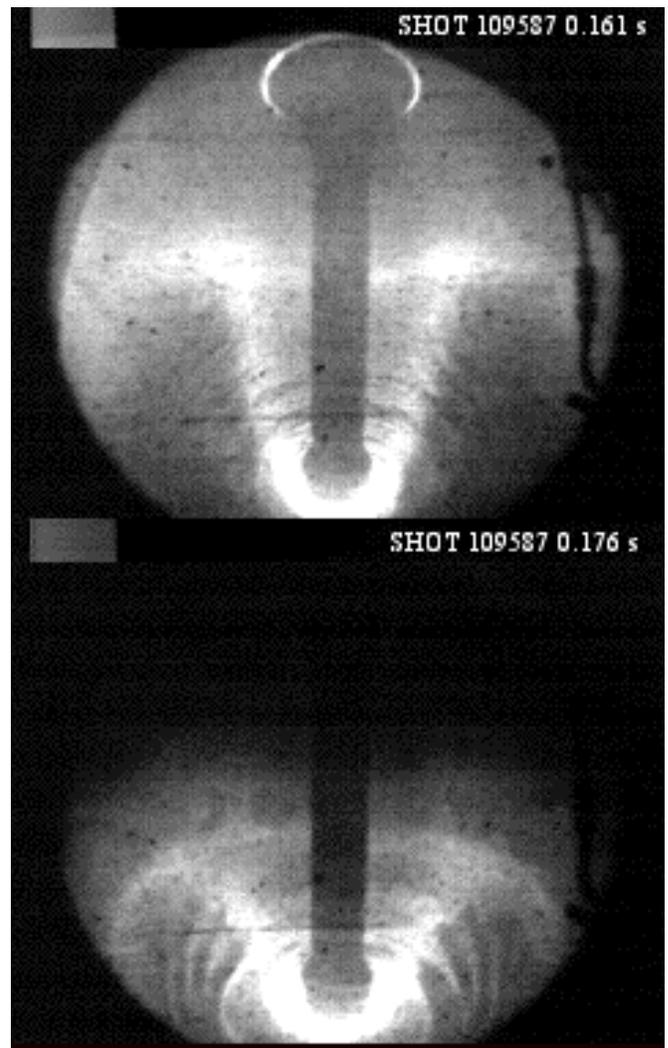


Figure 7. TV images before and during an absorber arc in NSTX after the insulator redesign. Note that there is no sign of a localized arc.

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