

4 MHD Equilibrium - One Dimensional

$$\left. \begin{array}{l} \text{① Equilibrium: } \frac{\partial}{\partial t} = 0 \\ \text{② Mostly without flow, } v = 0 \end{array} \right\} \Rightarrow -\nabla p + \frac{(\nabla \times B) \times B}{4\pi} = 0$$

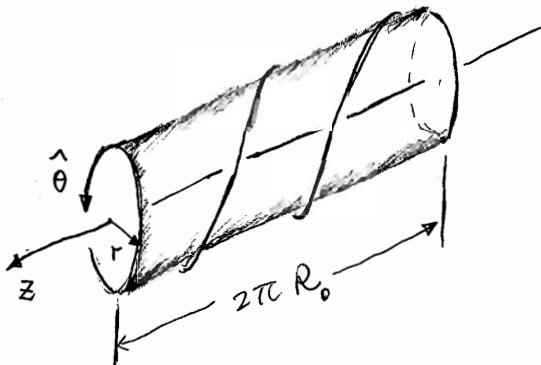
$\nabla \cdot B = 0$

Screw - pinch

4 Eqs. for 4 components

$$B = B_\theta(r) \hat{\theta} + B_z(r) \hat{z}$$

$$p = p(r)$$



$$\vec{j} = \frac{c}{4\pi} \nabla \times B$$

$$= J_\theta \hat{\theta} + J_z \hat{z}$$

$$J_\theta = -\frac{c}{4\pi} \frac{d}{dr} B_z(r)$$

$$J_z = \frac{c}{4\pi} \frac{1}{r} \frac{d}{dr} [r B_\theta(r)]$$

momentum Eq: $\frac{\vec{j} \times \vec{B}}{c} = \nabla P$ or $\frac{(\vec{j} \times \vec{B}) \times \vec{B}}{4\pi} = \nabla \vec{P}$

\Rightarrow

$$\frac{d}{dr} \left(P + \frac{B_\theta^2 + B_z^2}{8\pi} \right) + \frac{B_\theta^2}{4\pi r} = 0$$



Curvature

bending force

Two freedoms for $P(r)$, $B_\theta(r)$, $B_z(r)$

Question: MHD Eqs have 8 Eqs for 8 components, why

there are two freedoms for the screw pinch equilibrium?

safety Factor:

$$q(r) \equiv \frac{r B_z(r)}{R_0 B_\theta(r)}$$

How many turns in \hat{z} does the field line travel
for one turn in $\hat{\theta}$?

(one turn in $\hat{z} \equiv 2\pi R_0$ in \hat{z})

$$\frac{r d\theta}{dz} = \frac{B_\theta}{B_z} \Rightarrow \frac{dz}{2\pi R_0} = \frac{r B_z}{R_0 B_\theta} \frac{d\theta}{2\pi} \Rightarrow q = \frac{r}{R_0} \frac{B_z(r)}{B_\theta(r)}$$

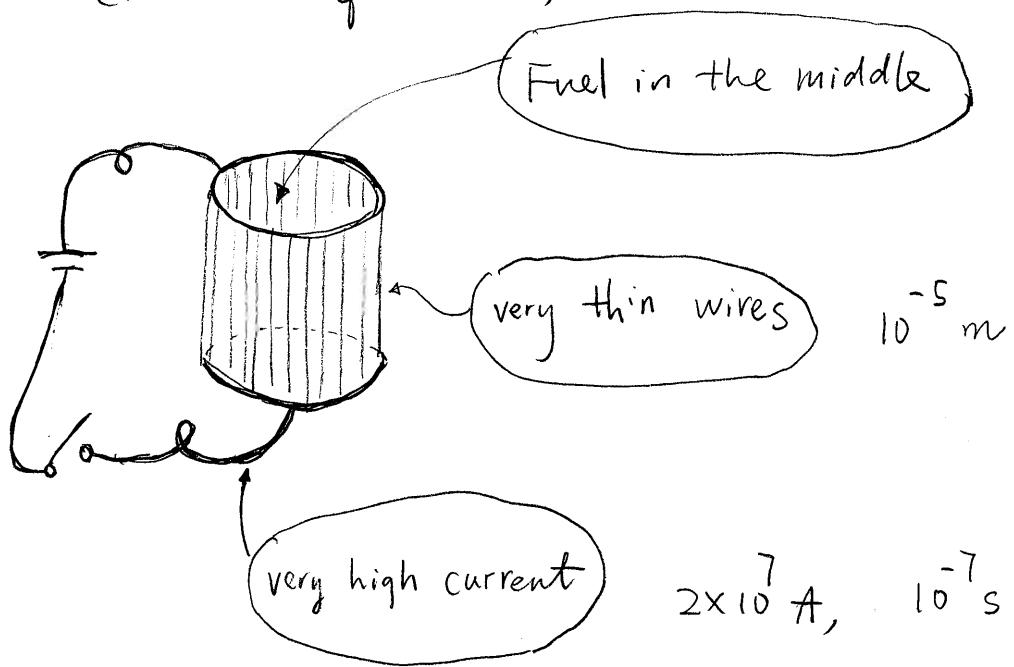
Z - Pinch

$$J_\theta = 0, \quad B_z = 0$$

$$q = 0 \quad \text{unsafe (unstable)}$$

z-pinch for inertial confinement

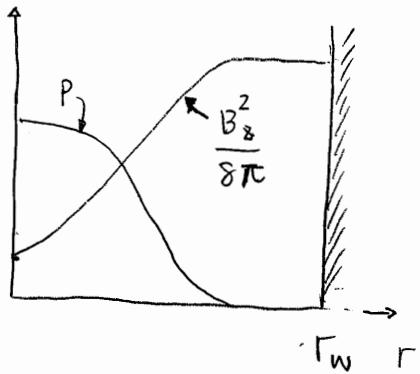
(not an equilibrium)



θ -Pinch

$$\bar{J}_B = 0, \quad B_\theta = 0$$

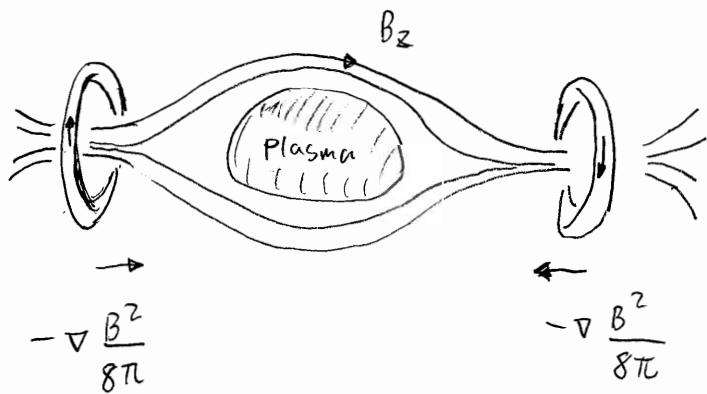
$$P + \frac{B_z^2}{8\pi} = \frac{B_0^2}{8\pi}$$



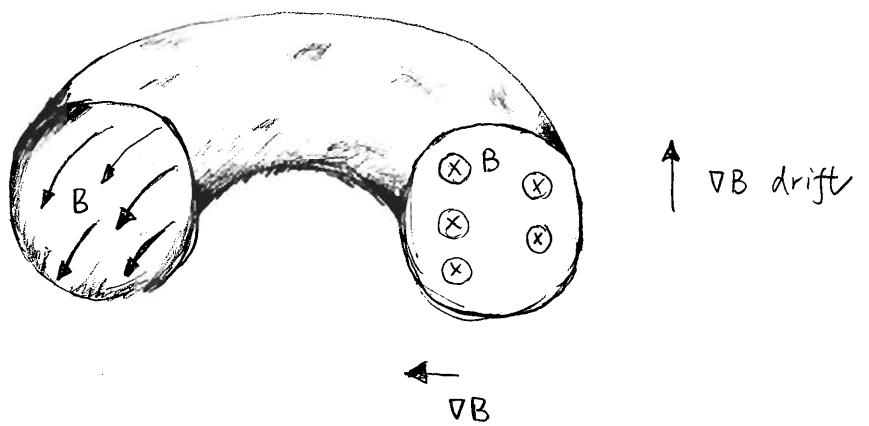
$q = \infty$, very safe (stable)

But, no axial confinement,

Solution ①: make a mirror machine. \Rightarrow 2D Equilibrium



solution (2). Make a toroidal magnetic field

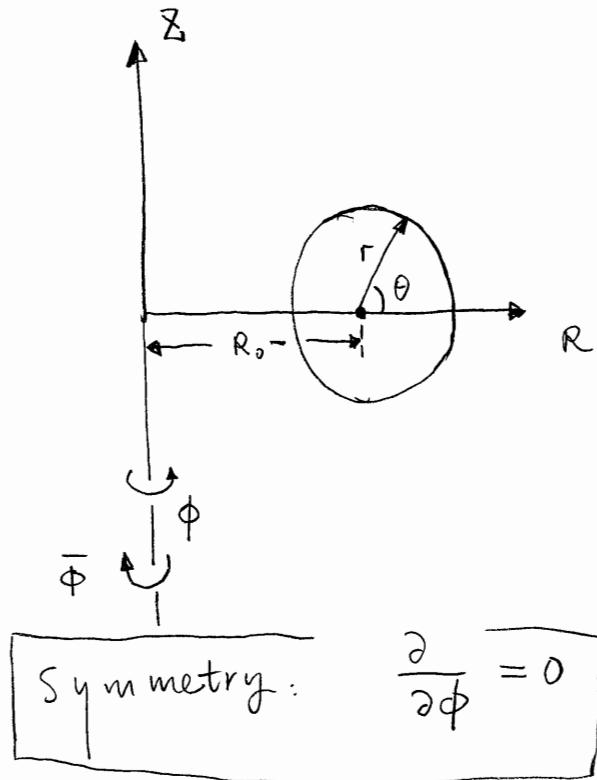


Need poloidal field to confine particle radially.

⇒ toroidal screw-pinch, (2D)

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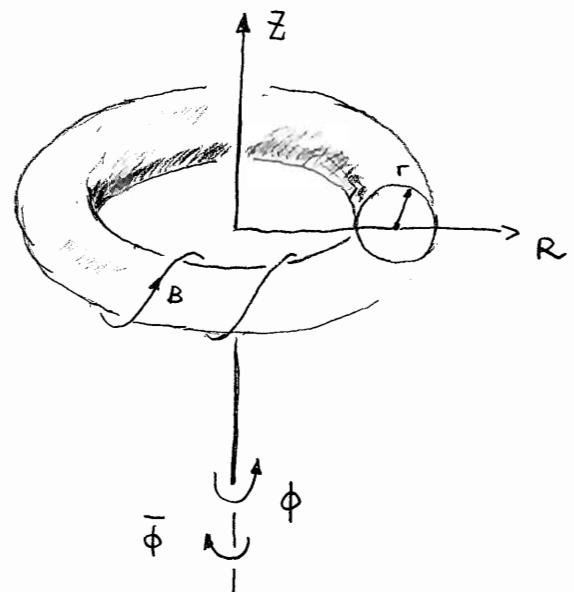
MHD Equilibrium 2D, Grad-Shafranov Eq.



Symmetry: $\frac{\partial}{\partial \phi} = 0$

cylindrical coord. (R, ϕ, Z)

toroidal coord. $(r, \theta, \bar{\phi})$



$$\mathbf{B} = \nabla \times \mathbf{A}$$

$$\Rightarrow \left\{ \begin{array}{l} B_R = - \frac{\partial A_\phi}{\partial Z} \\ B_Z = + \frac{1}{R} \frac{\partial}{\partial R} (R A_\phi) \end{array} \right. = \left\{ \begin{array}{l} - \frac{1}{R} \frac{\partial \psi}{\partial Z} \\ \frac{1}{R} \frac{\partial \psi}{\partial R} \end{array} \right. \quad (1)$$

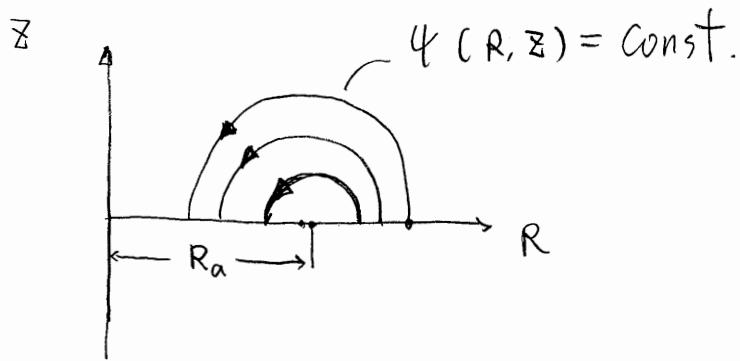
$$= \left\{ \begin{array}{l} - \frac{1}{R} \frac{\partial \psi}{\partial Z} \\ \frac{1}{R} \frac{\partial \psi}{\partial R} \end{array} \right. \quad (2)$$

$$\psi \equiv R A_\phi$$

$$\Rightarrow \vec{B} = \frac{1}{R} \nabla \psi \times \hat{e}_\phi + \vec{B}_\phi \quad \dots \quad (3)$$

$$\mathbf{B} \cdot \nabla \psi = 0 \quad \Rightarrow \quad \psi = \text{const} \quad \text{is a flux surface}$$

- The fundamental reason for the existence of magnetic flux surface is the symmetry, not $\nabla \cdot \mathbf{B} = 0$
- More on the Hamiltonian structure of magnetic field later.



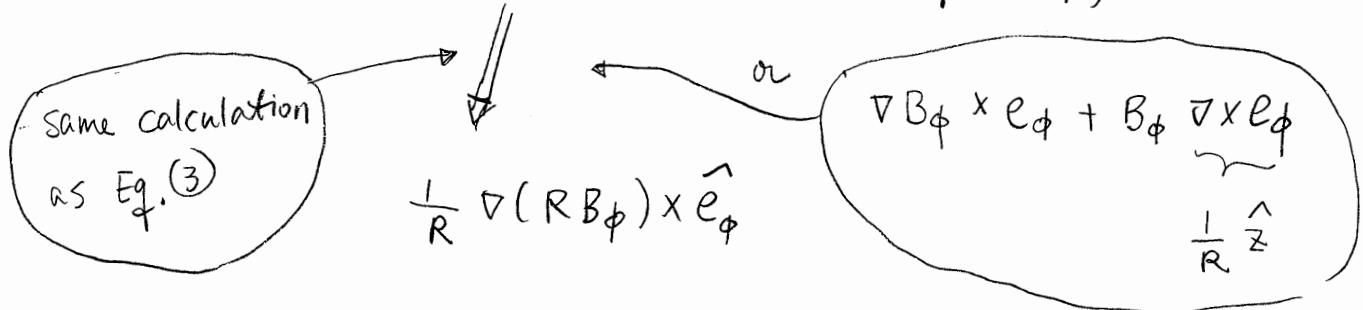
Assume: There is a magnetic axis at R_a

poloidal flux enclosed by a flux surface $\psi = \text{const.}$

$$\Psi_p = 2\pi \int_{R_a}^R dR R B_z(R, z=0)$$

$$= 2\pi [\Psi(R, z=0) - \Psi(R_a, z=0)]$$

$$\frac{4\pi}{c} \vec{j} = \nabla \times \vec{B} = \nabla \times (B_\phi e_\phi) + \nabla \times \left(\frac{\nabla \psi}{R} \times e_\phi \right)$$



$$\begin{aligned} \nabla \times \left(\frac{\nabla \psi}{R} \times e_\phi \right) &= \frac{\nabla \psi}{R} \cdot e_\phi - e_\phi \cdot \underbrace{\nabla \left(\frac{\nabla \psi}{R} \right)}_{\nabla \cdot \left(\frac{1}{R} \frac{\partial \psi}{\partial R} e_R + \frac{1}{R} \frac{\partial \psi}{\partial z} e_z \right)} + (e_\phi \cdot \nabla) \frac{\nabla \psi}{R} - \left(\frac{\nabla \psi}{R} \cdot \nabla \right) e_\phi \\ &= -e_\phi \left[\underbrace{\frac{1}{R} \frac{\partial^2 \psi}{\partial R^2} - \frac{1}{R^2} \frac{\partial \psi}{\partial R} + \frac{1}{R} \frac{\partial^2 \psi}{\partial z^2}}_{\frac{\partial}{\partial R} \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right)} \right] \\ &\quad - e_\phi \end{aligned} \tag{4}$$

$$= -e_\phi \frac{\Delta^* \psi}{R}$$

$$\Delta^* = R \frac{\partial}{\partial R} \left(\frac{1}{R} \frac{\partial \psi}{\partial R} \right) + \frac{\partial^2 \psi}{\partial z^2}$$

$$\frac{1}{4\pi} \left[\frac{1}{R} \nabla(RB_\phi) \times e_\phi - e_\phi \frac{\Delta^* \psi}{R} \right] \times \left[\frac{1}{R} \nabla \psi \times e_\phi + e_\phi B_\phi \right] = \nabla P \quad (5)$$

★

$$0 = B \cdot \nabla P = \frac{1}{R} e_\phi \cdot (\underbrace{\nabla P \times \nabla \psi}_{\parallel}) = \frac{1}{R} e_\phi \cdot \left(\frac{\partial P}{\partial \theta} \nabla \theta \times \nabla \psi \right)$$

$$\therefore \left(\frac{\partial P}{\partial \psi} \nabla \psi + \frac{\partial P}{\partial \theta} \nabla \theta \right)$$

$$\Rightarrow \frac{\partial P}{\partial \theta} = 0 \quad \Rightarrow \quad P = P(\psi)$$

assume: $e_\phi \cdot [\nabla \theta \times \nabla \psi] \neq 0$

★

$$0 = j \cdot \nabla P = \frac{1}{R} \left[e_\phi \cdot \nabla P \times \nabla(RB_\phi) \right] = \frac{1}{R} \frac{\partial P}{\partial \psi} \left[e_\phi \cdot \nabla \psi \times \nabla(RB_\phi) \right]$$

$$\Rightarrow RB_\phi = F(\psi)$$

$$(5) \Rightarrow -\frac{1}{4\pi} \frac{B_\phi}{R} F'(\psi) \nabla \psi - \frac{\Delta^* \psi}{4\pi R^2} \nabla \psi = \nabla P$$

$$\Rightarrow \boxed{\Delta^* \psi = -FF' - 4\pi R^2 P'} \quad \text{Grad-Shafranov Eq.} \quad (6)$$



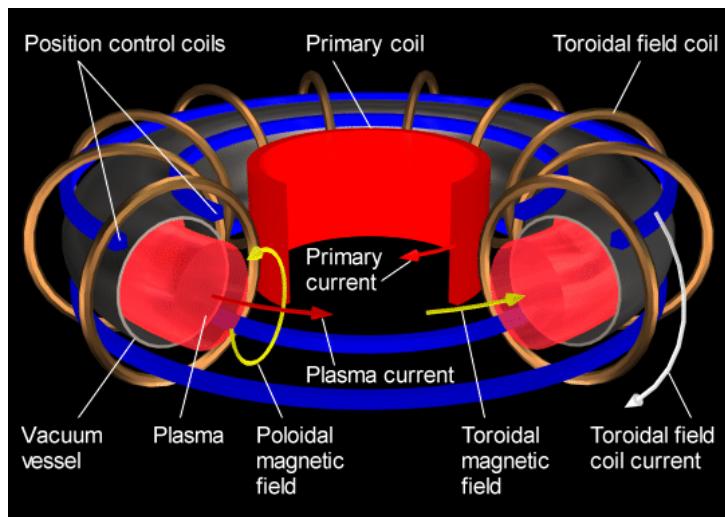
Harold Grad



Vitalii D. Shafranov

Grad-Shafranov Equation:

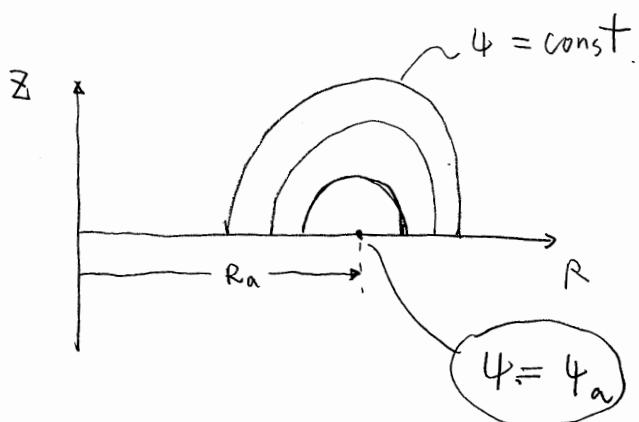
$$\Delta^* \psi = -FF' - 4\pi R^2 p'$$



specify $P(\psi)$, $F(\psi)$ and B.C.s

solve for $\psi(R, z)$. Again, two freedoms!

what is $F(\psi)$?



$$\vec{j} = \frac{C}{4\pi} \left[\frac{1}{R} \nabla F \times \hat{e}_\phi - \frac{\star \psi}{R} \hat{e}_\phi \right]$$

$\Rightarrow \psi = \text{const}$ is a current flux surface.

Polooidal current enclosed by a flux surface:

$$\begin{aligned} I_p &= 2\pi \int_{R_a}^R dR \ R j_z = \frac{C}{2} \int_{R_a}^R dR \ \nabla F \\ &= \frac{C}{2} \left[F(R, z=0) - F(R_a, z=0) \right] \quad (7) \\ &\quad \parallel \qquad \qquad \qquad \parallel \\ &\quad F(\psi) \qquad \qquad F(\psi = \psi_a) \end{aligned}$$

Safety factor q

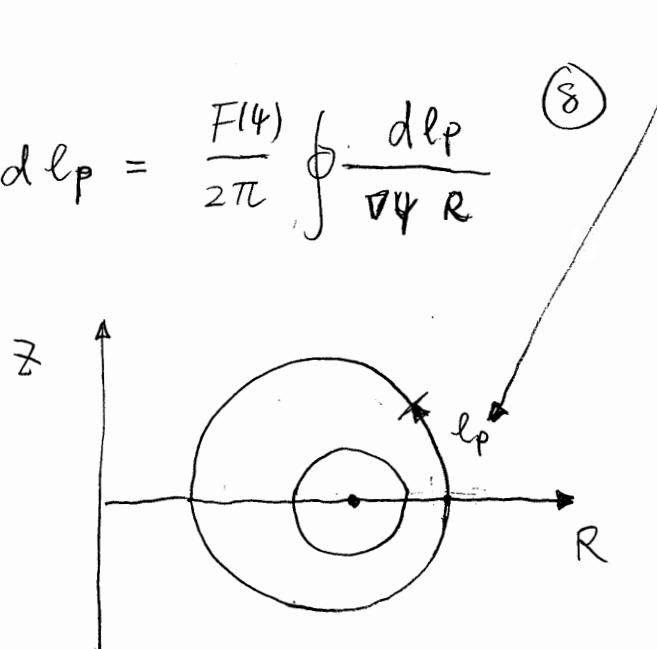
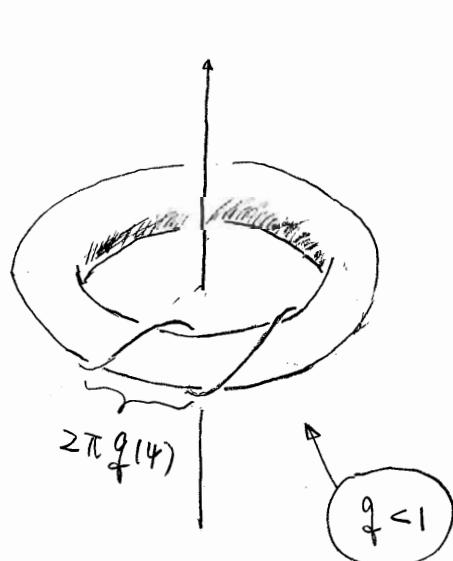
The local magnetic pitch angle $\frac{B_\phi}{B_p}$ is not a constant even on a flux surface. The safety factor q is defined as a flux function:

Number of toroidal transit in one poloidal transit on the flux surface.

$$\frac{R d\phi}{B_\phi} = \frac{d l_p}{B_p}$$

l_p : poloidal arc length
on the surface

$$q(\psi) = \frac{1}{2\pi} \oint \frac{B_\phi}{B_p R} d l_p = \frac{F(4)}{2\pi} \oint \frac{d l_p}{B_p R} \quad (8)$$

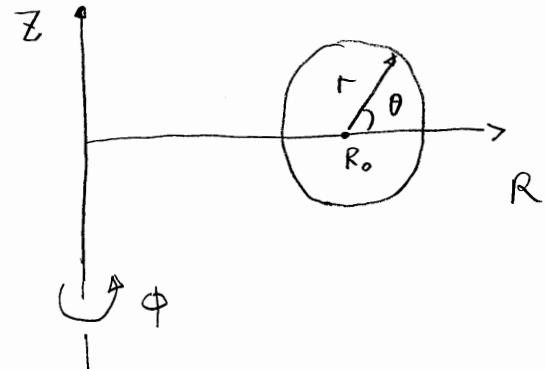


Equilibrium of low- β , large aspect ratio

Tokamak; solution of Grad-Shafranov Eq.

First: cylindrical coord \rightarrow toroidal coord.

$$\left\{ \begin{array}{l} R = R_0 + r \cos \theta \\ Z = r \sin \theta \\ \phi = -\bar{\phi} \end{array} \right.$$



$$\left\{ \begin{array}{l} \frac{\partial}{\partial r} = \cos \theta \frac{\partial}{\partial R} + \sin \theta \frac{\partial}{\partial Z} \end{array} \right. \quad (9)$$

$$\left\{ \begin{array}{l} \frac{\partial}{\partial \theta} = -r \sin \theta \frac{\partial}{\partial R} + r \cos \theta \frac{\partial}{\partial Z} \end{array} \right. \quad (10)$$

$$(9) \sin \theta + (10) \frac{\cos \theta}{r} \Rightarrow \left\{ \begin{array}{l} -\frac{\partial}{\partial Z} = \sin \theta \frac{\partial}{\partial r} + \frac{\cos \theta}{r} \frac{\partial}{\partial \theta} \end{array} \right. \quad (11)$$

$$(9) \cos \theta - (10) \frac{\sin \theta}{r} \Rightarrow \left\{ \begin{array}{l} \frac{\partial}{\partial R} = \cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \end{array} \right. \quad (12)$$

$$\begin{aligned}
\frac{\partial^2}{\partial z^2} &= \left[\sin\theta \frac{\partial}{\partial r} + \frac{\cos\theta}{r} \frac{\partial}{\partial \theta} \right] \left[\sin\theta \frac{\partial}{\partial r} + \frac{\cos\theta}{r} \frac{\partial}{\partial \theta} \right] \\
&= \sin^2\theta \frac{\partial^2}{\partial r^2} - \frac{\cos\theta \sin\theta}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\sin\theta \cos\theta}{r} \frac{\partial^2}{\partial r \partial \theta} \\
&\quad \frac{\cos^2\theta}{r} \frac{\partial^2}{\partial r^2} + \frac{\sin\theta \cos\theta}{r} \frac{\partial^2}{\partial r \partial \theta} \\
&\quad \frac{\cos^2\theta}{r^2} \frac{\partial^2}{\partial \theta^2} - \frac{\sin\theta \cos\theta}{r^2} \frac{\partial^2}{\partial \theta^2}
\end{aligned}$$

$$\begin{aligned}
\frac{\partial^2}{\partial R^2} &= \left[\cos\theta \frac{\partial}{\partial r} - \frac{\sin\theta}{r} \frac{\partial}{\partial \theta} \right] \left[\cos\theta \frac{\partial}{\partial r} - \frac{\sin\theta}{r} \frac{\partial}{\partial \theta} \right] \\
&= \omega^2 \theta \frac{\partial^2}{\partial r^2} + \frac{\sin\theta \cos\theta}{r^2} \frac{\partial^2}{\partial \theta^2} - \frac{\sin\theta \omega^2 \theta}{r} \frac{\partial^2}{\partial r \partial \theta} \\
&\quad \frac{\sin^2\theta}{r} \frac{\partial^2}{\partial r^2} - \frac{\sin\theta \cos\theta}{r} \frac{\partial^2}{\partial r \partial \theta} \\
&\quad T \frac{\sin^2\theta}{r^2} \frac{\partial^2}{\partial \theta^2} + \frac{\sin\theta \cos\theta}{r^2} \frac{\partial^2}{\partial \theta^2}
\end{aligned}$$

$$\frac{\partial^2}{\partial z^2} + \frac{\partial^2}{\partial R^2} = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}$$

$$\Delta^* \psi = -\frac{\partial^2 \psi}{\partial R^2} - \frac{1}{R} \frac{\partial \psi}{\partial R} + \frac{\partial^2 \psi}{\partial z^2}$$

$$= \frac{\partial^2 \psi}{\partial r^2} + \frac{1}{r} \frac{\partial \psi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2} - \frac{1}{R} \left(\cos \theta \frac{\partial \psi}{\partial r} - \frac{\sin \theta}{r} \frac{\partial \psi}{\partial \theta} \right)$$

(13)

ordering:

$$\textcircled{1} \quad \frac{r}{R} \sim \epsilon \ll 1 \quad \text{Large aspect ratio}$$

$$\textcircled{2} \quad \frac{B_p}{B_\phi} \sim \epsilon, \quad q \sim 1 \quad \text{Safe}$$

$$\textcircled{3} \quad \beta \sim \frac{P}{B_\phi^2} \sim \epsilon^2 \quad \text{low pressure}$$

Solution:

$$\psi \approx \psi_0(r) + \psi_1(r, \theta)$$

$$\dot{p}(\psi) = p'_2(\psi) \approx p'_2(\psi_0) + p''_2(\psi_0) \psi_1$$

$$F(\psi) = F_0 + F_2(\psi) \approx F_0 + F_2(\psi_0) + F_2(\psi_0) \psi_1$$

|| ||

$B_0 R_0$ $R_0 B_{\phi 2}(\psi_0)$

$$F(\psi) = F_2(\psi) = R_0 B'_{\phi 2}(\psi_0) + R_0 B''_{\phi 2}(\psi_0) \psi_1$$

Order $O(\epsilon^0)$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \Psi_0}{\partial r} = -4\pi R_o^2 P_2'(\Psi_0) - B_o R_o^2 B_{\phi 2}'(\Psi_0) \quad (14)$$

$$B_{\theta 1} = \frac{1}{R_o} \frac{d \Psi_0}{d r} \quad \text{---} \quad \downarrow$$

$$\frac{d}{dr} \left(P_2 + \frac{B_o B_{\phi 2}}{4\pi} \right) + \frac{B_{\theta 1}}{4\pi r} \frac{d}{dr} (r B_{\theta 1}) = 0$$

↑
Screw pinch

$$\frac{d (B_o B_{\phi 2})}{dr} = \frac{\partial}{\partial r} \left(\frac{B_\phi^2}{2} \right) + O(\epsilon^2)$$

Order $O(\epsilon)$:

$$\frac{\partial^2 \Psi_1}{\partial r^2} + \frac{1}{r} \frac{\partial \Psi_1}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \Psi_1}{\partial \theta^2} - \frac{1}{R_o} \left(\cos \theta \frac{\partial \Psi_0}{\partial r} \right)$$

$$= -4\pi R_o^2 P_2''(\Psi_0) \Psi_1 - 8\pi R_o \Gamma \cos \theta P_2'(\Psi_0)$$

$$- R_o^2 B_o B_{\phi 2}''(\Psi_0) \Psi_1 \quad (15)$$

$$\text{Let } \Psi_1(r, \theta) = \bar{\Psi}_1(r) \cos\theta,$$

$\cos\theta$ factors out in Eq.(15)

\Rightarrow

$$\frac{d^2 \bar{\Psi}_1}{dr^2} + \frac{1}{r} \frac{d\bar{\Psi}_1}{dr} - \frac{1}{r^2} \bar{\Psi}_1 = \frac{1}{R_0} \frac{d\Psi_0}{dr}$$

$$= -4\pi R_0^2 P_2''(\Psi_0) \bar{\Psi}_1 - 8\pi R_0 r P_2'(\Psi_0) - R_0^2 B_0 B_{\phi_2}'(\Psi_0) \bar{\Psi}_1 \quad (16)$$

Eg. (14) \Rightarrow

$$-4\pi R_0^2 P_2''(\Psi_0) - B_0 R_0^2 B_{\phi_2}''(\Psi_0) = \frac{1}{\Psi_0'} \frac{d}{dr} \left(\frac{1}{r} \frac{d}{dr} r \frac{d\Psi_0}{dr} \right)$$

$$B_{\theta 1} = \frac{1}{R_0} \frac{d\Psi_0}{dr}$$

$$\Rightarrow \frac{1}{r} \frac{d}{dr} \left(r \frac{d\bar{\Psi}_1}{dr} \right) - \frac{\bar{\Psi}_1}{r^2} = -\frac{\bar{\Psi}_1}{B_{\theta 1}} \frac{d}{dr} \left(\frac{1}{r} \frac{d}{dr} (r B_{\theta 1}) \right)$$

$$= -8\pi R_0 r P_2'(\Psi_0) + B_{\theta 1}$$

$$\times r B_{\theta 1}$$

$$\Rightarrow B_{\theta 1} \frac{d}{dr} \left(r \bar{\Psi}_1' \right) - \frac{\bar{\Psi}_1 B_{\theta 1}}{r} = \bar{\Psi}_1 r \frac{d}{dr} \left[\frac{1}{r} \frac{d}{dr} (r B_{\theta 1}) \right]$$

$$= -8\pi R_0 r^2 B_{\theta 1} P_2'(\Psi_0) + r B_{\theta 1}^2 \quad (17)$$

$$\begin{aligned}
 \text{LHS} &= B_{\theta 1} \bar{\Psi}'_1 + B_{\theta 1} r \bar{\Psi}''_1 - \frac{\bar{\Psi}_1 B_{\theta 1}}{r} \\
 &\quad - \bar{\Psi}_1 r \left[\frac{B'_{\theta 1}}{r} - \frac{B_{\theta 1}}{r^2} + B''_{\theta 1} \right] \\
 &= \left[B_{\theta 1} \bar{\Psi}'_1 - \bar{\Psi}_1 B'_{\theta 1} \right] + \left[B_{\theta 1} \bar{\Psi}''_1 - \bar{\Psi}_1 B''_{\theta 1} \right] r \\
 &= \frac{d}{dr} \left[r (B_{\theta 1} \bar{\Psi}'_1 - \bar{\Psi}_1 B'_{\theta 1}) \right] \\
 &= \frac{d}{dr} \left[r B_{\theta 1}^2 \frac{d}{dr} \left(\frac{\bar{\Psi}_1}{B_{\theta 1}} \right) \right]
 \end{aligned}$$

Finally, OCF eq 13:

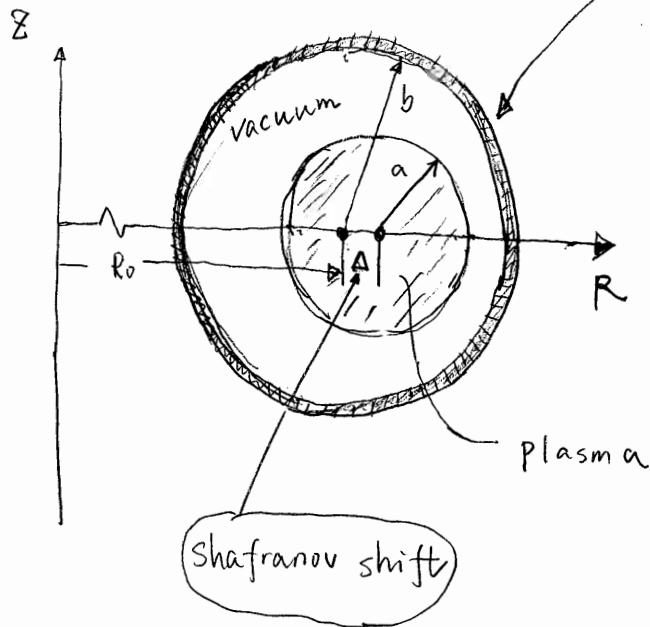
$$\frac{d}{dr} \left[r B_{\theta 1}^2 \frac{d}{dr} \left(\frac{\bar{\Psi}_1}{B_{\theta 1}} \right) \right] = r B_{\theta 1}^2 - 8\pi r^2 \frac{d P_2(\bar{\Psi}_o(r))}{d r}$$

(18)

Need B.C. to solve for $\bar{\Psi}_1$

B.C 1

perfectly conducting wall at $r = b$



$$\left\{ \begin{array}{l} \Psi(b, \theta) = \Psi_w \\ \Psi_0(b) = \Psi_w \\ \Psi_1(b, \theta) = 0 \end{array} \right.$$

$$\bar{\Psi}_1 = B_{\theta 1} \int_r^b \frac{dx}{x^2 B_{\theta 1}(x)} \int_0^x \left[8\pi y^2 \frac{dP_z(\Psi_0(y))}{dy} - y B_{\theta 1}^2(y) \right] dy \quad (19)$$

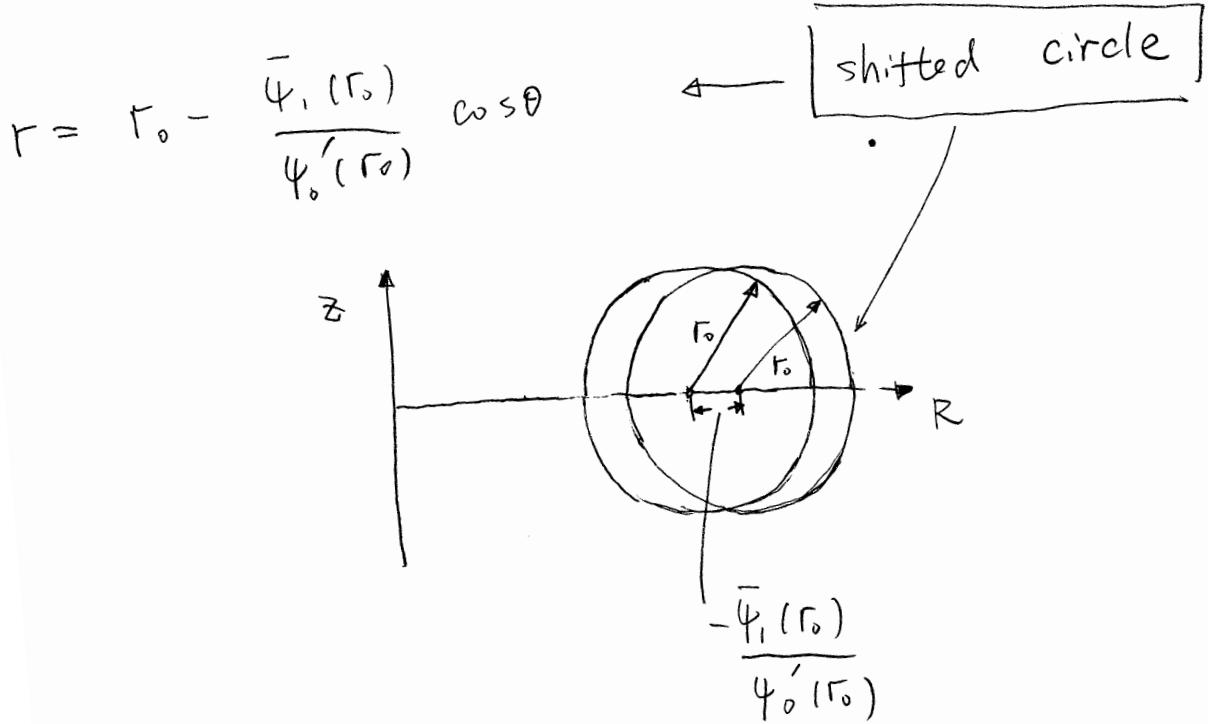
$$\Psi(r, \theta) = \Psi_0(r) + \bar{\Psi}_1(r) \cos \theta$$

$$\text{Flux surface } \Psi(r, \theta) = c \Rightarrow r(\theta) = r_0 + \Gamma_1(\theta)$$

$$0(t) : \quad \Psi_0(r_0) = c$$

$$0(\epsilon) : \quad \Psi'_0(r_0) \Gamma_1(\theta) + \bar{\Psi}_1'(r_0) \cos \theta = 0$$

$$\Rightarrow r_1(\theta) = - \frac{\bar{\psi}_1(r_0)}{\psi'_0(r_0)} \cos \theta$$



Shafranov shift: the shift of the plasma-vacuum boundary

$$r_a = a + \Delta \cos \theta$$

$$\Delta = - \frac{\bar{\psi}_1(a)}{\psi'_0(a)},$$

$$\bar{\psi}_1(a) = B_{01}(a) \int_a^b \frac{dx}{x B_{01}(x)} \left\{ \int_0^a \left[8\pi y^2 \frac{dP_2}{dy} - y^2 B_{01}^2(y) \right] dy \right.$$

$$+ \left. \int_a^x \left[-y B_{01}^2(y) \right] dy \right\}$$

$$B_{01}(r) = B_{01}(a) \frac{a}{r}, \quad r \geq a$$

a number
related to B_0

a number
related to B_0

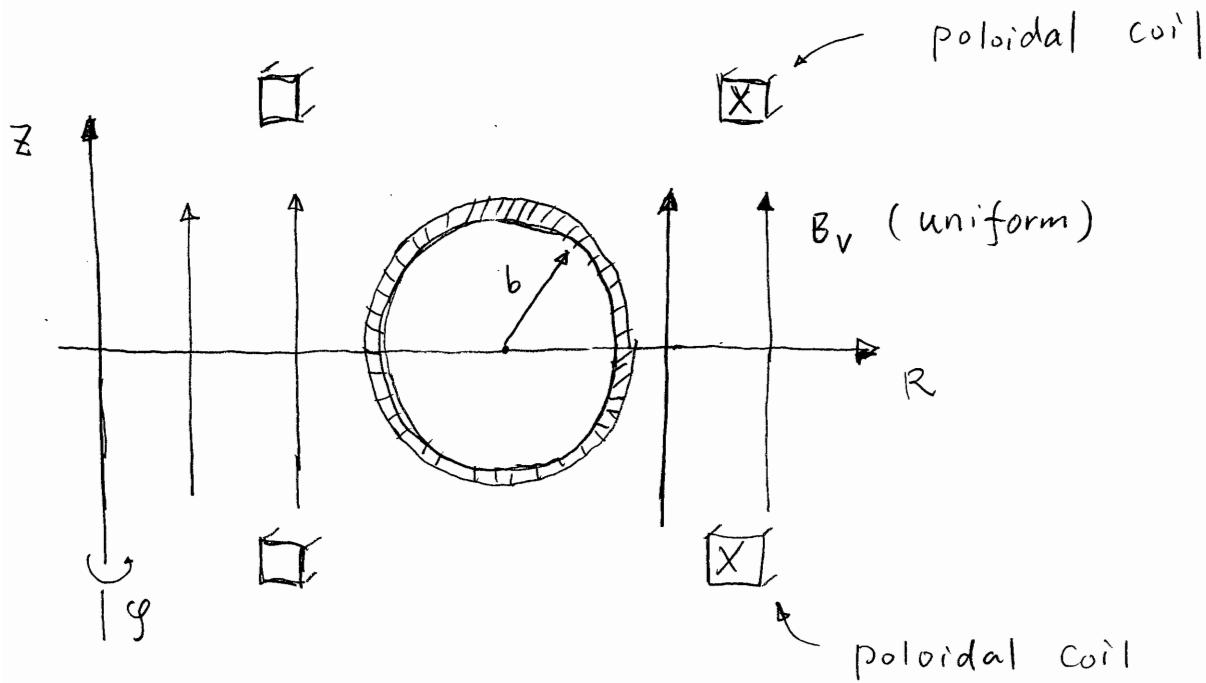
Over all,

$$\frac{\Delta}{b} = \frac{b}{2R_0} \left[\left(\beta_P + \frac{\ell_i - 1}{2} \right) \left(1 - \frac{a^2}{b^2} \right) + \ln \frac{b}{a} \right]$$

$$\beta_P = \frac{\int_0^a 2\pi r P dr}{\frac{B_{\theta 1}^2(a)}{8\pi} \pi a^2} = \text{poloidal beta}$$

$$\ell_i = \frac{1}{\pi a^2 B_{\theta 1}^2(a)} \int 2\pi r B_{\theta 1}^2 dr = \text{internal inductance}$$

[B.C. 2] : perfectly conducting wall at $r = b$,
 +
 external vacuum field B_v created by
 poloidal coils.



- Assume:
- ① The field inside the chamber does not leak out, because it's fast MHD activity
 - ② The vacuum field B_v penetrates in because it has been set up long enough.

$$\Psi_v = R_0 B_v r \cos \theta \quad (\text{why?})$$

$$B.C. \quad \Psi(b, \theta) = \Psi_w + R_0 B_v \cos \theta$$

$$\Rightarrow \Psi_0(b) = \Psi_w$$

$$\Psi_1(b, \theta) = R_0 B_v b \cos \theta$$

$$\Rightarrow \bar{\Psi}_1(b) = R_0 B_v b$$

$$\boxed{\bar{\Psi}_1 = \text{RHS of Eq.(19)} + R_0 B_v b \frac{B_{\theta 1}(r)}{B_{\theta 1}(b)}}$$

$$\Delta = -\frac{\bar{\Psi}_1(a)}{\Psi'_0(a)}$$

$$\Delta \rightarrow \Delta + \Delta_V,$$

$$\Delta_V = - \frac{R_0 B_v b}{\Psi'_0(a)} \frac{B_{\theta 1}(a)}{B_{\theta 1}(b)} = - \frac{B_v b}{B_{\theta 1}(b)}$$

↑
 $\boxed{\text{The vacuum field pushes plasma back!}}$